Best Practice Catalog

Main Power Transformer

Revision 2.0, 8/06/2012
Prepared by

MESA ASSOCIATES, INC.
Chattanooga, TN 37402

and

OAK RIDGE NATIONAL LABORATORY
Oak Ridge, Tennessee 37831-6283
managed by
UT-BATTELLE, LLC
for the
U.S. DEPARTMENT OF ENERGY
under contract DE-AC05-00OR22725
## Contents

1.0 Scope and Purpose..............................................................................................................4

1.1 Hydropower Taxonomy Position.......................................................................................4

1.1.1 Main Power Transformer Components .................................................................4

1.2 Summary of Best Practices............................................................................................7

1.2.1 Performance / Efficiency & Capability - Oriented Best Practices ......................7

1.2.2 Reliability / Operations & Maintenance - Oriented Best Practices ......................8

1.3 Best Practice Cross-references .....................................................................................10

2.0 Technology Design Summary........................................................................................11

2.1 Material and Design Technology Evolution..................................................................11

2.2 State of the Art Technology .........................................................................................12

3.0 Operations & Maintenance Practices ............................................................................14

3.1 Condition Assessment .................................................................................................14

3.2 Operations ...................................................................................................................15

3.3 Maintenance ................................................................................................................16

4.0 Metrics, Monitoring and Analysis..................................................................................23

4.1 Measures of Performance, Condition, and Reliability .............................................23

4.2 Integrate Improvements...............................................................................................24

5.0 Information Sources: ....................................................................................................25
1.0 Scope and Purpose

This best practice for the Main Power Transformer (MPT) discusses design components, condition assessment, operations, and maintenance best practices with the objective to maximize overall plant performance and reliability.

The primary purpose of the main power transformer is to step up the generator output to a higher voltage for efficient transmission of energy. The MPT is a critical component of any generation station. As the MPT connects the generator to the transmission grid, the output of the generator is directly dependent on the availability and operational status of the transformer. Thermal and electrical limits of the transformer must be considered for reliable long term operation. Proper design, operation, and maintenance are required to provide the utmost efficiency, performance and reliability of the hydro unit.

1.1 Hydropower Taxonomy Position

Hydropower Facility → Powerhouse → Power Train Equipment → Transformer

1.1.1 Main Power Transformer Components

The primary components of the MPT related to performance and reliability consist of a core, windings, dielectric insulation system, bushings, and external cooling system.

**Core**: The core functions to provide an optimal path for the magnetic flux and efficiently magnetically couple the windings. The core of a transformer is comprised of thin magnetic laminations stacked together and tightly clamped into place by a steel clamping structure. Each lamination is provided with a thin coating of insulating varnish to insulate each lamination from the adjacent lamination. On core form transformers, the clamping structure is electrically insulated from the core laminations and within the structure itself with one intentional core ground provided. The insulation of the laminations and clamping structure reduces eddy currents and unwanted circulating currents within the structure. Shell form transformers are not provided with a single point core ground by the nature of their design. Cores can be designed as either single phase or three phase configurations depending on capacity and user requirements.

**Windings**: The windings function as the conducting circuit for the transformer and consist of turns of insulated wire or cable which are placed around the magnetic core. Various configurations of winding construction and conductor transpositions are utilized to increase the efficiency of the windings. Each winding conductor and each winding assembly is insulating from one another as well as from ground potential. A primary and a secondary winding are used in a typical two-winding MPT. The alternating current that flows through the primary winding establishes a time-varying magnetic flux, some of which links to the secondary winding and induces a voltage across it. The magnitude of this voltage is proportional to the ratio of the number of turns on the primary winding to the number of turns on the secondary winding. This is known as the “turns ratio”. Most MPT’s are provided with a tap winding, typically part of the secondary high voltage winding, which connects winding leads to a tap
changer mechanism allowing the user to adjust the turns ratio to closely match the system voltage so as to prevent over-excitation of the transformer. The tap changer mechanism may be of the de-energized type (DETC) which can only be operated with the transformer completely de-energized or may be designed for on-load tap changing operation (OLTC). OLTC’s are far more complex devices, require additional maintenance, and add considerable cost to the transformer. The windings and tap configuration of a MPT allows the low voltage input to be converted to higher voltages providing for efficient transmission of electric power.

Dielectric Insulation System: The dielectric insulation system consists of both solid and liquid dielectric materials. The purpose of this system is to insure that the windings, conductors, and core remain electrically insulated from one another and from ground potential. The solid dielectric insulation system can consist of various materials including electrical grade cellulose, Nomex®, pressboard, wood, and insulating varnishes and films. The liquid insulation consists of an insulating fluid, normally a highly processed mineral oil, which provides for the dielectric properties and protection of the solid insulation as well as serving as the cooling medium for the transformer. The insulating oil minimizes oxidation of cellulose and serves as a deterrent for chemical attacks of the core and windings. The quality and life of the solid insulation system is highly dependent on the quality of the liquid insulating fluid.

Bushings: The function of the bushings is to provide a path for current flow from the windings inside the transformer to external connections while maintaining the dielectric integrity of the voltage-to-ground clearance required. A central conductor passes through an insulator which can consist of porcelain, resin, or polymer material. The inside of the bushing may contain paper and foil layers, film, or ink to create a low value capacitance to grade the voltage between the conductor and ground. Bushings may be filled with insulating oil or may be resin impregnated, particularly at higher voltages, and are known as capacitor type bushings. Capacitor type bushings are usually provided with a test or voltage tap to allow testing of the capacitor layers. Lower voltage bushings may consist of only a central conductor and an insulator.

External Cooling System: The purpose of the external cooling system is to remove the heat generated by power losses within the transformers and maintain operation of the components within design temperature parameters. The removal of heat protects the windings, core, and dielectric system from thermal degradation, critical for the reliability of the transformer. The heat losses are transferred to the insulating fluid which is circulated through external systems to remove the heat and return cooler fluid to the transformer. The external cooling system can be comprised of radiators, coolers, fans, motor driven pumps, and/or water cooled heat exchangers based on the design and capacity requirements of the transformer.
Non-performance, but reliability related components of a MPT include the tank, oil preservation system, and controls/protective devices.

**Tank:** The purpose of the tank is to provide a sealed container to house the core, winding assembly, and the insulating fluid. The tank is usually made of welded steel construction and is provided with removable inspection covers. The bushings are mounted to the tank for electrical connection of the transformer windings to external bus. Auxiliary equipment such as controls, protective devices, oil preservation systems, and cooling system components are usually attached to the tank.

**Oil Preservation System:** The purpose of the oil preservation system is to prevent moisture, atmospheric air, and other contaminants from entering into the tank and contaminating the insulating system. This minimizes oxidation and deterioration of the dielectric insulation system both chemically and electrically. There are various types of oil preservation systems including gas sealed, pressurized inert gas sealed, free breathing, and sealed conservator type systems.

**Controls/Protective Devices:** Controls and protective devices are equipment required for operation of the transformer. Instrumentation is also part of the control system. They provide for manual and automatic control of the cooling system, monitoring of temperatures, on-line monitoring (i.e. dissolved gas and moisture), trip and alarm functions, and power supply transfers. The controls are usually housed in a cabinet mounted to the transformer and are connected to the various devices. The protective devices can vary based on the user’s specifications and include such items as pressure relief devices, rapid rise fault pressure relays, temperature monitors, various on-line monitors, and lock out systems for tap changers.
1.2 Summary of Best Practices

1.2.1 Performance / Efficiency & Capability - Oriented Best Practices

The performance levels of the MPT can be defined as follows:

The Installed Performance Level (IPL) is the performance capabilities of the transformer determined during OEM factory testing and at commissioning. These capabilities may be validated by comparison of factory test reports and field electrical test data prior to initially placing the transformer in service.

The Current Performance Level (CPL) is determined by an accurate analysis of the transformers operating characteristics. These would include thermal performance at full load as well as component condition or test deviations or limitations discovered.

Determination of the Potential Performance Level (PPL) typically requires interface with vendors for new transformer design, loss information, and cost in order to evaluate the achievable performance potential of replacement transformer(s).
Best Practices include:

- Routine testing to verify performance within the original design criteria and factory test baseline data.
- Maintain operation of the transformer within its thermal and capacity limits.
- Insure that temperature and loading limits are maintained by operation personnel and that alarms are responded to in a timely manner. Winding temperatures should be constantly monitored and trended. Increased temperature trends should be investigated to determine cause.
- All alarms and/or trips should be investigated and considered valid until proved otherwise.
- Real-time monitoring and analysis of transformer performance at Current Performance Level (CPL) to detect and mitigate deviations from design parameters for the Installed Performance Level (IPL) due to system degradation, thermal issues, or malfunction of instrumentation.
- Maintain documentation of IPL and update if major modifications are performed (e.g., winding replacement, cooling system upgrades, oil reclamation).
- Periodic comparison of the CPL to the IPL to monitor deterioration and trigger maintenance or repair. This is especially important regarding routine field electrical test results and oil analysis.
- Trend transformer performance and test data for early detection of deterioration, contamination, thermal degradation, and incipient faults.
- Include industry acknowledged choices and experience for transformer design, replacement components, and maintenance practices to plant engineering standards.

1.2.2 Reliability / Operations & Maintenance - Oriented Best Practices

- Establish a comprehensive dissolved gas-in-oil analysis (DGA) testing program to monitor the internal health of the transformers insulation system, as well as other components. Accurate analysis and trending of analytical data can provide early detection of thermal and electrical incipient faults, insulation degradation, and allow for intervention and mitigation measures. On-line monitors are available for real time analysis.
- Maintain an insulating oil quality testing program to timely monitor the chemical and electrical condition of the insulating fluid. Degradation of the insulating fluid leads to degradation of the solid insulation system which can lead to failure. Enhanced testing processes for furanic compounds, particle analysis, dissolved metals, corrosive sulfur, etc. can assist in determining life and maintenance
criteria. It should be understood that the life of the insulation system is the life of the transformer.

- Insure that a dry insulation system is maintained. When indicated, appropriate and efficient field dry out processes should be used.

- Implement a routine field electrical testing program and track and trend critical data. Establish action limits to correct defects found during tests prior to placing the transformer back in-service. Thoroughly document findings and corrective action taken.

- Implement a thermographic inspection program and trend results of individual components and families.

- Insure operation of the MPT within its design voltage limits, typically 105% sustained to avoid damaging over-excitation issues. Adequate voltage taps should be provided to adjust to any feasible system condition to prevent this situation.

- Consider specification limits on new transformers on allowable flux density. Modern transformer designers typically design to 110% maximum of nominal voltage. Some user specifications will place limits on the allowable flux density at this elevated excitation voltage. One user requires 1.7 Tesla maximum at 110% nominal voltage.

- Operate the transformer within its thermal design limits to prevent accelerated thermal aging and damage to the winding and lead insulation system and bushings.

- Investigate all oil or nitrogen leaks and determine the need and priority for repair.

- Maintain the cooling and oil preservation system with a preventative maintenance program as these systems protect the transformer from damaging heat, moisture, and atmospheric air.

- Consider modernizing free breathing oil preservation systems to sealed conservator systems

- Consider replacing desiccant breathers with maintenance free breathers on conservators and OLTC’s

- Use on-line OLTC systems to maintain improved integrity of the insulating fluid and internal OLTC components.

- Trend bushing condition and replace when significant deterioration is indicated by comparing all electrical test values to individual bushing nameplate data. Replace
bushings with known high risk for failure rates. On-line bushing monitors can provide real time bushing condition.

- Recondition or reclaim insulating oil when trend analysis indicates need. Develop specifications for the type and grade of insulating oil to be used in user’s transformer.

- Test and calibrate controls and indicating devices and upgrade when required.

- Insure availability of on-site or system wide spare transformer(s) and spare parts to reduce the forced outage time incurred with a failure. Availability of spare transformers also greatly assists in scheduled replacement of aged transformers minimizing outage time.

- Monitor for trends of deteriorating condition of the transformer (decrease in Condition Indicator (CI)) and decrease in reliability (an increase in Equivalent Forced Outage Rate (EFOR), a decrease in Effective Availability Factor (EAF). Adjust maintenance and capitalization programs to correct deficiencies.

1.3 Best Practice Cross-references

- I&C - Automation Best Practice
- Electrical – Generator Best Practice
2.0 Technology Design Summary

2.1 Material and Design Technology Evolution

Transformers have changed very little since their inception with regard to their functionality; however, considerable improvements have been made in component materials. The principal change is the efficiency and performance of modern core designs and improved windings and insulation materials. Modern transformers are smaller, have higher thermal limits and fewer losses than the older transformer fleet. Advancements in core materials, winding design and maintenance innovations have improved efficiency and reliability significantly.

Transformer efficiency is primarily determined by the original design criteria. Incremental efficiency improvements may be accomplished by system upgrades, but winding and core replacement are often not cost effective for very old transformers. Attempting to install a modern core or windings in an existing tank also limits design criteria. The transformers insulation condition, loading profile, historic ambient conditions, age, and known risks are among the top factors in an assessment to determine whether the MPT is a candidate for replacement or rehabilitation.

Analysis of operational history and test data may indicate that the CPL has significantly deviated from the IPL. Increased maintenance and operational constraints are also used to determine the CPL.

Many older transformers were more liberally designed and losses were not evaluated as critically as today. These losses can be significantly higher than those of a modern transformer. Losses associated with the MPT can be grouped into three major categories.

- Load losses
- No-load losses
- Auxiliary losses

The load losses are the largest of the three followed by the no-load losses. The auxiliary losses are comparatively quite small. For example, typical losses for a 36 year old MPT rated 161-13.2-kV, 58,500/78,000/87,300 kva, three phase, 55°C/65°C rise, ONAN/ONAF are:

- Load losses 212.57 kW at rated current
- No-load losses 56.07 kW at 100% rated voltage
- Auxiliary losses 3 kW with all fans in operation

The load losses are associated with the windings and primarily consist of:

- $I^2R$ loss associated with current
- Eddy current loss in the winding conductors
Advanced technology in winding conductor arrangements, transposition, and materials are used today in modern designs to reduce these losses. As the name implies, these losses are governed by the load current carried by the transformer and the resistance of the windings.

The no-load losses are associated with the core but independent of the load for the most part, and they are incurred whenever the transformer is energized. These losses are primarily the result of:

- Excitation current
- Hysteresis loss
- Eddy currents

The auxiliary losses are associated primarily with the cooling system and are incurred by the pump motors and fan motors and are usually negligible in comparison to load and no-load losses.

2.2 State of the Art Technology

More efficient material and manufacturing techniques have been developed over the years to reduce the no-load losses. Modern transformer designers can utilize various grades of steel for the core laminations. Fabrication techniques such as laser scribing were not available years ago. Improved core assembly and configuration processes are also utilized in modern transformers. Figure 2 shows an example of a modern core in a manufacturing facility. Figure 3 illustrates a 3-phase winding assembly before installation in the tank.

Figure 2: Modern Core during Manufacturing
Excitation current can be reduced by specifying limits on allowable flux density. One user recommends 1.7 Tesla maximum at the 110% of nominal voltage.

Sound pressure levels can be reduced with modern transformer design with reduced flux density and sound limits. Limits are set by NEMA based upon an equivalent two-winding transformer. Sources of noise are typically magnetostriction in the core and the cooling system equipment. By adding a requirement for new transformers to be 6 dB (A) less than the NEMA limits and using the above limit on magnetic flux levels, the sound pressure levels can be significantly reduced. These improvements will be appreciated by operations and maintenance personnel working in close proximity to the transformers and does not add appreciable cost to the initial price of the MPT.

Advancements in instrumentation and controls can now provide for more efficient and reliable monitoring of the transformer and associated systems. These include fiber optics for actual winding conductor temperature, bearing wear monitors for motor driven oil pumps, partial discharge probes, and on-line bushing monitors.

Replacement of aged MPT’s with modern state of the art designs may result in significant reduction of losses as compared to those of 40-50 year old transformers. The cost savings should be considered for the life cycle of a new transformer and decisions should not be based solely on initial costs. Additionally, establishing partnering agreements with manufacturers and developing standardized designs can result in substantial cost savings in the purchase cost of replacement transformers and reduce inventory of spare parts.
3.0 Operations & Maintenance Practices

3.1 Condition Assessment

Once the MPT is properly assembled, oil filled, processed, and energized, its life cycle begins. A reliable life cycle is determined by how well the MPT is operated, maintained, and protected from faults. Reliability and loss prevention of the IPL and CPL are directly related to proper operation and maintenance of the MPT.

The ability to elicit good history lays the foundation for a good assessment. In order to provide for a representative condition assessment of the MPT, the first step is information gathering. Initial data includes: DGA, oil quality, factory tests, routine electrical tests, thermographic tests, operational history, maintenance history, and fault history. Component failure and replacement as well as any major upgrades or repairs is important information to review. Interviews with maintenance personnel can provide excellent information on current and past issues. Conduct a problem oriented evaluation based on existing and potential issues. Depending on the frequency of test cycles, it may be useful to review the last 15-20 years of test results and history. The quality of the data directly relates to the quality of the condition assessment. Trending and analysis of all data sources are performed to determine past experience and current health of the MTP.

DGA data is one of the most valuable diagnostics for determination of the internal health of the transformer. Overheating of the oil and cellulose, partial discharge, sparking/arcing, and decomposition of cellulose materials can be monitored, detected, and trended to reflect internal reactions occurring within the transformer. The rate of generation and magnitude of individual dissolved gases are both important factors to consider in analysis. The magnitude of concentrations can depend on age, operating history, and design.

The quality of the oil and its maintenance plays an important part in the life of the insulation system. Insulating oil degrades in time and the degradation by-products can have a considerable negative effect on the paper insulation as well as degradation of the papers dielectric performance level. Accelerated aging and loss of insulation strength can occur if the oil is not properly maintained. Periodic analysis of the oil quality tests data detects adverse conditions and allows for planned oil maintenance when required.

Various electrical tests can validate the integrity of the MPT. Insulation power factor tests can assist in determination of the winding insulation as well as that of the bushings. Winding resistance tests can detect problems in tap changer contacts, poor connections (bolted or brazed) and broken conductor strands within the windings. Analysis of electrical test data is an important tool to assist in determination of the transformers electrical integrity. Trending of the test results is invaluable in determining the degree and rate of degradation.

Thermographic inspections and analysis can provide a wealth of information ranging from low oil levels and overheating in bushings and connections to component malfunction such as poor heat transfer in radiators and coolers. A thorough review of thermal data provides yet another tool for condition assessment. Figure 4 is an example of a thermographic image detecting a bushing problem.
The age of the transformer must be considered as it relates to the condition of the insulation system. In the presence of heat, moisture, and oxygen, all cellulose insulation systems will deteriorate. This degradation process is cumulative and cannot be reversed. The insulation strength will weaken until the system cannot adequately perform its intended electrical function. Even with excellent maintenance, these three entities can be minimized, but not entirely eliminated. Replacement of the entire insulation system for a 35-40 year old transformer is not economically feasible. Age plays an important factor in the condition assessment of MPT’s.

After or during the data process, a physical inspection of the MPT is necessary in order to form a current impression of the equipment and discover any existing anomalies. Nameplate information can be obtained during the inspection. A systematic inspection process for the condition assessment should be performed to include the main tank, cooling system, bushings, oil preservation system, tap changer, controls, and protective/indicating devices.

Upon completion of the data assessment and physical inspection, a systematic and consistent approach should be used for each MPT. This allows prioritization to be assigned to each MPT for ranking purposes which assists in developing a plan for rehabilitation or replacement options assisting in both short term and long term strategic planning.

### 3.2 Operations

The MPTs operational parameters are governed by the original design criteria. Operation within these parameters provides the most efficient performance of the equipment and provides for optimum service life.
All transformers have thermal limits that must be strictly observed in order to maximize the life of the transformer. These temperature rise ratings are typically 55°C for standard cellulose insulation or 65°C for thermally upgraded cellulose. These temperature rise ratings are based on an average 30°C ambient over a 24 hour period. These ratings also determine the set points for the first and second stage cooling equipment if provided. Elevated operating temperatures above design ratings will cause excessive deterioration of the insulation system. For every 10°C increase in windings hot spot temperature above the design, the solid insulations reliable service life is cut in half. Thermal decomposition is cumulative and the life of the transformer is the life of the insulation system.

The MPT’s apparent power capacity must equal or exceed that of the generator output within the prescribed power factor limits. This capacity is determined during design and any anticipated future uprates to the generator need to be considered when initially sizing the transformer. Sustained overloading can have significantly adverse consequences and cause damage to the windings, core, and insulation system. Overloading can also cause excessive temperature rise to occur in sealed bushings and lead to failure. The MPT should be operated within its design capacity in order to maximize the service life.

The maximum continuous operating voltage as governed by ANSI C84.1-1995 and IEEE C57.1200 is 105% continuous secondary voltage at rated MVA and at a power factor not less than 0.8. The system conditions may require tap changer adjustments higher than the system voltage for regulation purposes. The primary voltage must be carefully maintained by the generator so as not to over excite the primary winding. Over excitation will allow the excitation current to increase exponentially and core saturation can occur leading to damage to the transformer.

Modern surge arresters should be used to protect the transformer from close in faults. Metal oxide surge arresters provide better protection than the older thyrite type. A best practice is to have the arresters mounted as close to the bushing terminals as practical. Most modern designs now mount the arrester assembly to the transformer tank.

Plants should, as a good practice, carefully monitor the transformers operational data and insure that strict controls are in place to prevent operation of the MPT beyond its intended design.

Provisions for spare transformers greatly enhance unit availability by providing “insurance” when a failure occurs. Major repairs or replacement of an MPT can be a costly and lengthy process and on-site spare transformers can significantly improve the availability factor for the unit when a major event occurs.

Utilization of fixed fire protection and oil containment systems can also reduce collateral damage and minimize environmental issues during a major failure event and should be considered as a good practice.

### 3.3 Maintenance

Preventative and corrective maintenance are essential components of any MPT. The demand for timely maintenance becomes more critical as the transformer ages. Routine maintenance...
of the various transformer components is vital to the life of any power transformer regardless of its age. An example of a typical maintenance issue would involve the inspection of the main tank. It should be inspected for oil leaks, rust, and effectiveness of the paint system. All gasketed flanges, mounting plates, bushing turrets, manhole covers, fittings, and valves should be inspected and oil leaks documented. Some oil leaks discovered may have severe consequences if not corrected. For instance, oil leakage on the intake side of a motor driven oil pump or flange can draw atmospheric air bubbles into the transformer. Bubble formation can be extremely detrimental to the electrical integrity of the transformer. Oil leaks should be corrected to address potential reliability and environmental concerns. Any unusual or excessive noise or vibration should be thoroughly investigated to determine source. Figure 5 illustrates one user’s remedial measures to mitigate an oil pump leak. Such measures are not recommended as a long-term repair.

![Figure 5: Excessive Oil Leak on Motor Driven Oil Pump](image-url)
Cooling system effectiveness requires all components to be fully functional. This includes cleanliness of air space between radiators and coolers as well as surface area. Shut off valves should be verified to be in the proper position and secured in place. All fans should be in place and be fully operational. Repair or replace fans and fan blades as required. Motor driven oil pumps should be checked for vibration, excessive noise, and balanced phase currents. As the motor of the oil pumps is immersed in oil, excessive overheating of the motor can generate combustible gas which will enter the transformer. Defective bearings can allow the pump impeller to come in contact with the casing ring and discharge small particles of metal inside the transformer. The cooling system must be maintained in good working order to preserve the thermal limitations of the MPT.

The bushings are a vital part of the MPT and have a direct impact on reliability and availability. They are internally connected to the windings by various schemes such as bolted connections, draw leads, and draw rods. Many high voltage bushings consist of an oil impregnated, multi-layer condenser wound on a central tube or rod. The condenser acts as a voltage divider and grades the line voltage to ground. Lower voltage bushings may be a condenser type or simply a fixed conductor through an insulator. Many older low voltage bushings used a compound or plastic filler within the insulator which may contain excessive levels of Poly Chlorinated Biphenols (PCBs) presenting environmental issues if a failure occurs. Routine tests, such as power factor, capacitance, hot collar, and thermographic inspections should be performed and all data referred back to the original nameplate data to identify potential risks. Trend results and replace bushings when out of tolerance limits are indicated. Inspections of bushings for poor connections, hot spots, proper oil levels, oil leaks, or insulator contamination/defects should be performed and documented. Bushings older than 30 years should be carefully monitored as they are at a higher risk for failure based on thermal aging. Low voltage bushings enclosed in housings are exposed to greater thermal stress. A single bushing failure can lead to a catastrophic transformer failure. Figure 6 clearly shows the damage caused from a single 500-kV bushing failure. This transformer was a total loss.
Figure 6 – Results of single 500-kV Bushing Failure

Figure 7 illustrates an example of an oil filled bushing, in this case contaminated with PCBs which can create environmental issues if a bushing failure occurs.

Figure 7: PCB Contaminated Bushings
The oil preservation system keeps external contaminates such as atmospheric air and moisture from entering the transformer. This protects both the liquid and solid insulation system. Oxidation of the oil is minimized and ingress of moisture is prevented. Preserving the oil quality is paramount to maximizing the life of the insulation system. A number of different type systems are used including sealed inert gas, inert gas constant positive pressure, free breathing, and sealed conservator. The function and operation of each type system used should be thoroughly understood in order to perform proper maintenance.

The two most common types of sealed tanks used on modern transformers in the U.S. are pressurized inert gas sealed and sealed conservator. The inert gas constant positive pressure sealed system (often referred to as nitrogen blanketed) maintains positive pressure of dry inert gas, usually nitrogen, above the oil. A nitrogen bottle and regulator system maintains a positive pressure of 0.5 to 5.0 PSI above the oil. The nitrogen used should meet ASTM D-1993 Type III with a -59°C dew point as specified in IEEE C-57.12.00. Regular inspection should be performed of the high pressure gauge, high/low pressure regulators, valves, pressure vacuum bleeder, and oil sump. Never allow the tank pressure to be zero or negative pressure. The sealed conservator system uses an expansion tank (conservator) which is mounted above the main tank and maintains the oil at atmospheric pressure. An air cell or diaphragm is placed inside the conservator which is vented through a dehydrating desiccant or maintenance free breather. As the oil in the main tank expands and contracts within the conservator, the transformer “breathes” to atmosphere via the breather. The air cell or diaphragm serves as a barrier and prevents any external air or other contaminates from coming into contact with the oil. The desiccant breather dries the air entering the conservator and the indicating desiccant gel should be inspected regularly and the desiccant replaced when approximately one-half of the material changes color. A maintenance free breather eliminates the need for desiccant replacement. The inspection port on top of the conservator should be removed every 5-6 years and the inside of the air cell or diaphragm inspected. If any oil is observed, a leak has developed, and the cell or diaphragm must be replaced. The quality of the insulating oil is highly dependent on proper maintenance of this system.

The quality of the insulating oil affects the health and life of the MPT. This highly processed mineral oil must be maintained or reduction in the dielectric strength and accelerated aging will be experienced by the insulation system. It is imperative that an aggressive oil testing program be in place for testing the chemical and electric characteristics of the oil. Standard tests and criteria are recommended and listed in IEEE C57.106. By performing trend analysis of the data, planned corrective action can be implemented before significant deterioration occurs. Many additional tests can be performed such as particle count, dissolved metals, oxidation inhibitor, corrosive sulfur, and furanic analysis to further refine the assessment of the oil and determine the maintenance techniques required. All mineral oils are organic compounds and will degrade over time. However, early detection of degradation allows for treatment of the oil in the field. Reconditioning of the oil will remove moisture, gases, and most particulates from the oil. Reclamation of the oil removes moisture, aging by-products, gases and particulates from the oil. Oil reclamation can return service aged oil to a pristine condition and may be both technically and economically a best practice for large MPTs. If
additives for inhibited oil and passivators for corrosive sulfur mitigation are used, they are sacrificially consumed over time and must be replenished.

The controls, indicators, and protective devices are usually mounted on the main tank. The control cabinet contains power supply transfer components, breakers, relays, switches, controls and terminal blocks for the auxiliary equipment for the transformer. The cabinet should be provided with weather tight seals, filtered louvers for dust removal and air circulation, and a strip heater to prevent condensation. Routine inspections should be performed to check for corrosion, water leakage, and component function. Thermographic inspections should be performed to check for poor connections and overheating of wiring and components. Oil flow and oil level indicators should be checked for proper operation including alarm contacts. Pressure relief devices (PRD) are mounted on the transformer tank cover and are a last defense to attempt to mitigate a tank rupture under major fault conditions and should be routinely inspected. The piping system for the PRD should be arranged to direct vented materials from the PRD away from operations personnel, particularly in the control cabinet area. When replacing these devices, verify the correct pressure setting of the PRD required since various pressure settings are available. Top oil temperature indicators provide remote monitoring and alarms functions and should be regularly tested and calibrated. Winding (hot spot) temperature indicators simulate the calculated hottest spot within the windings. These indicators provide for monitoring, alarm/trip, and cooling system control functions. Older type hot spot indicators are basically a dial type remote thermometer which is monitoring a heated well. The heated well in the presence of the transformer oil when located at a height on the tank wall approximate to the design location of the winding hot spot, will simulate a corresponding winding hot spot temperature as a function of winding current. Modern electronic control monitors are available that can provide all functions of the dial types plus additional features for computation and trending the transformer temperatures. Fiber optics are also available for measuring actual winding conductor temperatures in lieu of simulated values. The IEEE and EPRI have developed computational algorithms which are able to calculate rather than simulate the winding hot spot.

Rapid pressure or sudden pressure relays are normally used on MPTs to provide for rapid tripping of the transformer in the event of an internal fault. Many utilities have installed redundant relays with two out of three logic controls to eliminate single point tripping which greatly improves reliability and availability. All controls, indicators, and protective devices should be regularly inspected, tested, and calibrated as recommended by manufacturer’s specifications.

An aggressive routine electrical test program should be implemented allowing maintenance decisions to be data driven. As a minimum, the test program should include the following tests: winding power factor, bushing power factor and capacitance, bushing hot collar, winding resistance, excitation, core ground insulation resistance (if external), and insulation resistance. Thermographic inspections should be included within the test program. All data analysis should be referred back to base line commission and/or factory and nameplate data.
Additional advanced testing may be performed such as sweep frequency response analysis, acoustical and partial discharge tests when indicated.

The spare transformer(s) should be maintained in fully operational condition and should always be immediately available. Components should not be removed and used as spare parts for other MPT’s. When the spare is needed, it is usually installed under tight time constraints. Routine testing and inspections should be performed in the same manner as an operating transformer. Adequate critical spare parts such as bushings should be immediately available.
4.0 Metrics, Monitoring and Analysis

4.1 Measures of Performance, Condition, and Reliability

The fundamental efficiency of a main power transformer and associated losses is described below.

Where:
- $T_L$ is the total loss for the transformer (Watts)
- $N_L$ is the no-load loss at rated voltage (Watts)
- $L_L$ is the load loss at rated current (Watts)
- $A_L$ is the sum of the auxiliary losses (Watts)
- $O_P$ is the output of the transformer (Watts)
- $VA$ is the rated capacity of the transformer (Volt-ampere)
- $PF$ is the power factor of the secondary load

Total transformer losses are: $T_L = N_L + L_L + A_L$

Transformer output is then expressed as: $O_P = VA \times PF$

Transformer efficiency is given by: $\%\text{Efficiency} = (O_P / (O_P + T_L)) \times 100$

The condition of the MPT can be assessed by the Condition Indicator (CI) as defined according to HAP Condition Assessment Manual.

Industry reliability and availability statistics can be monitored and compared to unit performance by use of the North American Electric Reliability Corporation’s (NERC) performance indicators, such equivalent availability factor (EAF) and equivalent forced outage factor (EFOR). These are universally used by the power industry. Many utilities supply data to the Generating Availability Data System (GADS) maintained by NERC. This database of operating information is used for improving the performance of electric generating equipment. It can be used to support equipment reliability and availability analyses and decision-making by GADS data users.

Data Analysis of test data can be performed with the assistance and guidelines provided by various standards and guidelines related to specific analysis required. IEEE C57.104 and C57.106 standards provide information for testing and analysis of insulating oil. Various ASTM standards provide testing procedures and methodology. Several companies offer valuable electrical testing, oil analysis and investigation resources and provides assistance on interpretation and analysis techniques. Many vendor and reference materials are also available on all aspects of power transformers.

Determine the MPT’s existing capabilities (CPL) and compare results to previous or original test data (IPL). Assess the efficiency, reliability, capacity needs, transformer energy losses, and revenue loss. Compare results to new MPT design data (from transformer manufacturer), and determine potential efficiency, capacity, annual energy loss savings, and revenue gain (PPL). For the latter, calculate the installation/rehabilitation cost and internal rate of return to determine major upgrade or replacement justification.
The condition assessment of the MPT is quantified through the CI as derived according to HAP Condition Assessment Manual. The overall CI is a composite of the CI derived from each component of the transformer. This methodology can be applied periodically to monitor existing transformers and can be monitored and analyzed over time to determine condition trends that can impact performance and reliability.

The reliability of a unit as judged by its availability to generate can be monitored through reliability indexes or performance indicators as derived according to NERC’s Appendix F, Performance Indexes and Equations.

4.2 Integrate Improvements

The periodic field test results should be used to update the unit performance characteristics (CPL). These can be integrated into computer programs to provide on-line analysis results and anomalies to all involved personnel. Parameters can be established to trigger various maintenance or immediate action activities as required. Data trends allow predictive maintenance to be performed in lieu of reactive maintenance.

As the condition of the MPT changes over time, the CI and reliability indexes are trended and analyzed. Using this data, projects can be ranked and justified in the maintenance and capital programs to return the transformer to an acceptable condition and performance level or indicate the need for replacement for long term reliability and unit performance.
5.0 Information Sources:

Baseline Knowledge:
2. USBR, FIST Volume 3-30, Transformer Maintenance, October 2000
5. EPRI, Increased Efficiency of Hydroelectric Power, EM 2407, June 1992
7. EPRI, EL-2443, Vol. 1, Basic Transformer Life Characteristics

State of the Art
9. CIGRE WG12, 18, Report on Transformer Life Assessment, 2003
10. ORNL, HAP Condition Assessment Manual
11. Doble Client Committee on Circuit-Breakers and Bushings, Bushing Field Test Guide, Document BG661
12. EPRI, Transformer Aging as a Function of Temperature, Moisture, and Oxygen, 1013931, 2007

Standards:
15. IEEE C57.12.00, Standard General Requirements for Liquid Immersed Distribution, Power, and Regulating Transformers
16. IEEE C57.12.10, Standard Requirements for Liquid-Immersed Power Transformers
17. IEEE C57.91, Guide for Loading Mineral-Oil Immersed Transformers
18. NEMA Standard TR 1
19. IEEE 637, Guide for Reclamation of Insulating Oil and Criteria for Its Use

It should be noted by the user that this document is intended only as a guide. Statements are of a general nature and therefore do not take into account special situations that can differ significantly from those discussed in this document.
For overall questions
please contact:

Brennan T. Smith, Ph.D., P.E.
Water Power Program Manager
Oak Ridge National Laboratory
865-241-5160
smithbt@ornl.gov

or

Qin Fen (Katherine) Zhang, Ph. D., P.E.
Hydropower Engineer
Oak Ridge National Laboratory
865-576-2921
zhangq1@ornl.gov